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(11) EP 0 738 909 A1

(12)

EUROPEAN PATENT APPLICATION

(43) Date of publication:
23.10.1996 Bulletin 1996/43

(51) Int. Cl.⁶: G02B 6/38, G02B 6/34,
G02B 26/02

(21) Application number: 96105950.8

(22) Date of filing: 16.04.1996

(84) Designated Contracting States:
DE FR GB

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(30) Priority: 21.04.1995 JP 120625/95

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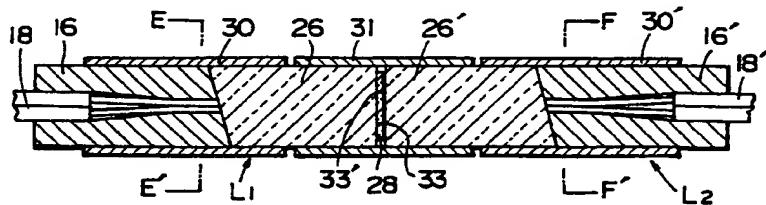
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(54) Optical fibre ferrule and optical coupler constructed using the optical fibre ferrule

(57) Provided are an optical fiber ferrule (16) holding a multiple of fibers and an optical coupler using the ferrule. A 4-core optical fiber ferrule (16) according to the present invention is constructed such that optical fibers are inserted into and fixed in a terminal end hole of the ferrule (16) so that the respective ends of four uncovered optical fibers closely adjoining one another are exposed and the terminal end is polished into a surface slightly inclined by an angle θ with respect to a surface perpendicular to the axis of the ferrule (16). The optical coupler comprises: first and second optical fiber ferrules (16, 16') each constructed as the above; first and second distributed refractive index optical lenses (26, 26') each having one end surface polished to have

an inclination θ with respect to the optical axis thereof; a mirror coating layer which reflects a portion of and transmits another portion of a light beam incident thereon; and a holding means (30, 30', 31) for bringing the respective inclined surfaces of the first ferrule (16) and the first distributed refractive index rod lens (26) into close contact to each other, bringing the respective inclined surfaces of the second ferrule (16') and the second distributed refractive index rod lens (26') into close contact to each other, disposing the mirror coating layer between the first and second distributed refractive index lenses (26, 26'), and coaxially holding these components.

F I G. 6



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Description**BACKGROUND OF THE INVENTION****1. Field of the Invention**

The present invention relates to an optical fiber ferrule and an optical coupler using the optical fiber ferrule.

2. Description of the Related Art

Among the known optical couplers are: an optical wave demultiplexer/multiplexer (WDM) in which a multiplexed light beam consisting of two wavelengths, passing through a single optical fiber is demultiplexed into two different optical fibers, or different rays of different wavelength respectively passing through two optical fibers are multiplexed and guided through a single optical fiber; and an optical branching/coupling device for distributing a light beam passing through a single optical fiber into two optical fibers at a desired ratio or, conversely, for combining different rays in two optical fibers into a single optical fiber.

Fig.10 is a sectional view containing the optical axis of a conventional optical coupler using a distributed refractive index rod lens. This optical coupler is a 1x2 circuit optical wave demultiplexer/multiplexer.

Distributed refractive index rod lenses 1, 2 constitute a convergent lens unit having an axial length $Z_1 = Z_2 = 0.25$ pitch. It should be noted that one end surface 3, 4 of each distributed refractive index rod lens is polished to have a surface inclined by 8 to 12° with respect to a plane perpendicular to its optical axis, thereby reducing the optical losses due to reflection. A mirror coating 6 having a desired reflecting and transmitting rate is applied onto the surface of a glass plate 5. The glass plate 5 is bonded to be fixed between end surfaces 7, 8 of the respective distributed refractive index rod lenses 1, 2.

Through holes 10, 11 are provided at a center portion of a ferrule 9 and optical fibers A, B are inserted into and adhered to the through holes to form a 2-core ferrule.

A through hole 13 is provided at the center of a ferrule 12 and an optical fiber C is inserted and adhered thereto to form a single core ferrule.

Also, terminal end surfaces 14, 15 of the 2-core ferrule 9 and single core ferrule 12 are similarly polished to have a surface inclined by 8 to 12° with respect to a plane perpendicular to the optical axis.

Fig.11 shows cross sections vertical to the optical axis of the respective portions of the above described coupler.

Here, it is supposed that the distance between optical axes O_1, O_2 of the optical fibers A, B attached to the 2-core ferrule 9 is $2r$, the optical axis of the optical fiber C of the single core ferrule 12 is O_3 and the optical axis of the distributed refractive index rod lenses 1, 2 is O .

The position of the optical axes O_1, O_2 of the optical fibers A, B attached to the 2-core ferrule 9 is fixed so that their respective distance from the optical axis O of distributed refractive index rod lens 1, 2 is r , and the optical axis O_3 of the optical fiber C of the single core ferrule 12 is fixed so that its distance from the optical axis O of distributed refractive index rod lens 1, 2 is r . It should be noted that fixing by adhesion to the inclined end surface 3 of the distributed refractive index rod lens 1 must be done with a precise positioning so as to achieve an accurate correspondence on a normal line YY' which passes through the center of the optical axes O_1, O_2 of the optical fibers A, B attached to the 2-core ferrule 9.

Supposing that the mirror coating 6 transmits a wavelength λ_1 and reflects a wavelength λ_2 , an incidence of a light beam containing wavelength components λ_1, λ_2 from the optical fiber A results in the wavelength component λ_1 being branched to the optical fiber C as transmitted through the mirror coating 6 and the wavelength component λ_2 being branched to the optical fiber B as reflected by the mirror coating 6. Conversely, by reversing the direction of light beams, a ray of wavelength λ_2 in the optical fiber B and a ray of wavelength λ_1 in the optical fiber C may be multiplexed into the optical fiber A. In other words, it is possible to construct a 1x2-circuit optical-wave demultiplexer/multiplexer.

The optical axis O_3 of the optical fiber C of the single core ferrule 12 must be secured with an accurate positioning in rotational adjustment such that its distance from the optical axis O of the distributed refractive index rod lens 2 is r and that it accurately coincides with a point on the normal line YY' passing through the center of the optical axes O_1, O_2 of the optical fibers A, B which are attached to the 2-core ferrule 9.

The excessive losses in an optical coupler of the above described type is greatly affected by the mechanical assembling accuracy in connecting the optical fibers A, B, C to the distributed refractive index lenses 1, 2. An alignment must be performed such that the positioning error in the respective bonded radius r of the optical fibers A, B, C from the optical axis O of the distributed refractive index rod lens 1, 2 is $2 \mu\text{m}$ or less.

Further, as a convenient assembling method with adjusting the optical axes of the optical fibers A, B, C with respect to the center optical axis of the distributed refractive index rod lens 1, 2, it is also possible to consider a method of automatically adjusting the optical axes based on the outer diametrical surface of the respective components as the reference by setting the outer diameter of the 2-core ferrule 9 to the same as the outer diameter of the distributed refractive index rod lens 1, 2 and aligning them along a V-shaped groove. It is, however, prerequisite to regulate the decentering of the two through holes 10, 11 provided in the 2-core ferrule 9 with respect to the outer diameter thereof to $1 \mu\text{m}$ or less. This is very difficult to be achieved using the current processing technologies.

One of the reasons for this is that, while it is necessary to hold the two sides of one center hole at the center of a machine to define a processing reference for the outer diametrical polishing in order to remove the eccentricity of a through hole with respect to the outer diameter of the ferrule, no means can be provided for setting such reference plane for the outer diametrical processing when two holes exist at the center portion.

Furthermore, the single core ferrule 12 is aligned to a position eccentric by radius r from the optical axis O of the distributed refractive index rod lens 2 after the aligned assembly of the 2-core ferrule 9 and the distributed refractive index rod lens 1, and must be subjected to an angular rotational adjustment to achieve a coincidence with the optical axis of the optical fiber of the 2-core ferrule 9. The processing becomes complicated and requires a skill, many man-hours and much manufacturing costs.

SUMMARY OF THE INVENTION

It is a first object of the present invention to provide an optical fiber ferrule which may be easily manufactured and be used in an optical coupler of the type as described above.

It is another object of the present invention to provide an optical coupler of which an adjustment in the assembling process is very easy.

It is a further object of the present invention to provide an optical coupler of which an adjustment in the assembling process is very easy and which may accommodate a large number of optical circuits.

To achieve the above objects, an optical fiber ferrule according to the present invention is constructed such that optical fibers are inserted into and fixed in a hole at a terminal end of the ferrule so as to expose the respective ends of four uncovered optical fibers closely adjoining one another and the terminal end is polished into a surface slightly inclined by an angle θ with respect to a plane perpendicular to the axis of the ferrule.

In the above described optical fiber ferrule, the following relation holds between the inner diameter of the ferrule and the outer diameter of the uncovered optical fiber and the angle of inclination θ may be set to 8 to 12°:

$$d = (2^{1/2} + 1)d_1 + \delta$$

where d is the inner diameter of the ferrule, d_1 is the diameter of each uncovered optical fiber and δ represents an error.

An optical coupler according to a first aspect of the present invention comprises:

first and second optical fiber ferrules each having optical fibers inserted into and fixed in a hole at a terminal end of the ferrule so as to cause the respective ends of four uncovered optical fibers closely adjoining one another to be exposed, the

terminal end being polished into a surface slightly inclined by an angle θ with respect to a plane perpendicular to the axis of the ferrule;

5 first and second distributed refractive index rod lenses each having one end surface polished to have inclination θ with respect to the optical axis thereof;

10 a mirror coating layer reflecting a portion of and transmitting another portion of a light beam incident thereon; and

15 a holding means for bringing the respective inclined surfaces of the first ferrule and the first distributed refractive index rod lens into close contact to each other, bringing the respective inclined surfaces of the second ferrule and the second distributed refractive index rod lens into close contact to each other, disposing the mirror coating layer between the first and second distributed refractive index lenses, and coaxially holding these components.

20 In the above described optical coupler, the outer diameter of the ferrule and the outer diameter of the distributed refractive index lens may be substantially the same so that the holding means is provided as a circular cylinder having a corresponding inner diameter.

25 It is another object of the present invention to provide an optical fiber ferrule in which N (an even number of 6 or larger) uncovered optical fibers are fixed in close contact to the inner circumference at an terminal end of the ferrule by inserting an auxiliary rod into the center thereof so as to position the optical fiber cores on a concentric circle, and the following relations hold among the ferrule terminal end inner diameter, the diameter of each uncovered optical fiber and the 30 outer diameter of the auxiliary rod:

$$d_N = d_1[(1/\sin(\pi/N)) + 1] + \delta$$

$$d_0 = d_1[(1/\sin(\pi/N)) - 1]$$

35 where d_N is the inner diameter of the ferrule, d_1 is the diameter of each uncovered optical fiber, d_0 is the outer diameter of the auxiliary rod; and δ represents an error.

An optical coupler according to the second aspect 40 of the present invention comprises:

the above described first and second optical fiber ferrules;

first and second distributed refractive index optical lenses;

a mirror coating layer reflecting a portion of and transmitting another portion of a light beam incident thereon; and

45 a holding means for bringing the first ferrule and first distributed refractive index rod lens into close contact to each other, bringing the second ferrule and the second distributed refractive index rod lens into close contact to each other, disposing the mirror coating layer between the first and second dis-

$$d = (2^{1/2} + 1)d_1 + \delta$$

tributed refractive index lenses, and coaxially holding these components.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig.1 is a sectional view of a first embodiment of optical fiber ferrule according to the present invention.

Fig.2 is an enlarged view showing the relation between a terminal end hole of the optical fiber ferrule and the respective ends of optical fibers.

Fig.3 shows a sectional view showing the state of connecting the above optical fiber ferrule and a distributed refractive index rod lens.

Fig.4 is a sectional view showing an embodiment of second aligning sleeve which forms a part of the holding means of an embodiment of an optical coupler according to the present invention.

Fig.5 is a sectional view of a mirror coating and a glass plate for supporting the mirror coating to be used in a first embodiment of optical coupler according to the present invention.

Fig.6 schematically shows the first embodiment of optical coupler according to the present invention.

Fig.7 illustrates the relation between the opposing optical fibers in the embodiment of Fig.6.

Fig.8 is a sectional view of a second embodiment of optical fiber ferrule according to the present invention.

Fig.9 is a sectional view showing an embodiment of optical coupler using the optical fiber ferrule as shown in Fig.8.

Fig.10 is a longitudinal sectional view of a conventional optical coupler.

Fig.11 shows sections respectively along a plurality of planes that are perpendicular to the optical axis of the conventional optical coupler as shown in Fig.10.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

The present invention will now be described in more detail with reference to the drawings.

Fig.1 is a sectional view of a first embodiment of optical fiber ferrule according to the present invention; and Fig.2 is an enlarged view showing the relation between a terminal end hole of the optical fiber ferrule, and the ends of uncovered optical fibers.

A through hole 17 having an inner diameter $d = 303 \mu\text{m}$ and a hole 19 for the insertion of optical fiber covering 18 are provided at a center portion of a ferrule 16. The through hole 17 and the stepped hole 19 are connected to each other through a taper surface 20 having an angle of inclination of 15° or less.

Denoted by numerals 21, 22, 23, 24 are four optical fibers each having an outer diameter $d_1 = 125 \mu\text{m}$ with the sheath 18 being removed.

The relation between diameter d of the center through hole 17 of the 4-core ferrule 16 and the diameter of each uncovered optical fiber satisfies the following equation:

where d_1 is the diameter of each uncovered optical fiber and δ represents an error.

By setting diameter d of the through hole in this manner, the uncovered optical fibers 21, 22, 23, 24 may be smoothly inserted therein as shown in the end view such that they tightly adjoin one another at their outer diametrical surface and at the same time are in contact with the inner diametrical surface of the through hole 17.

Thereafter, they are bonded by means of an adhesive and an end surface 25 is polished into a surface inclined by 8 to 12° with respect to a plane perpendicular to the optical axis. In this manner, at least two 4-core, optical fiber incorporated ferrules F_1 and F_2 are made.

If the inner diameter of through hole 17 $d = 303 \mu\text{m}$ and the outer diameter of uncovered optical fiber $d_1 = 125 \mu\text{m}$ as described above, the positions of optical axis r of the respective uncovered optical fibers 21, 22, 23, 24 with respect to the center axis are calculated to be 88.39 to $89.00 \mu\text{m}$. The error in radius position with respect to each other becomes a very small value of $0.3 \mu\text{m}$ and may be ignored. Similarly, an error in the angular phase in the circumferential direction is $2.2 \mu\text{m}$ which is not a problem in practice.

Further, since the 4-core ferrule 16 is constituted by a relatively wide single-center through-hole 17, the two end faces of the through hole may be held at the center of a lathe to be used as the processing reference in polishing the outer diameter. It is thus possible to achieve a precision in processing where both the precision in the outer diameter and the eccentricity of the through hole with respect to the outer diameter may be respectively controlled to $1 \mu\text{m}$ or less. It is preferable that the outer diametrical precision of the distributed refractive index rod lens be previously processed and corrected to be within $\pm 1 \mu\text{m}$.

An embodiment of optical coupler according to the present invention using the above described optical fiber ferrule will now be described with reference to Figs.3 to 7.

Fig.3 is a sectional view showing the state where the above described optical fiber ferrule and a distributed refractive index rod lens are connected to each other. The distributed refractive index lens 26 is a convergent lens unit having the axial length of the rod lens of 0.25 pitch. One end surface 27 of the distributed refractive rod lens 26 is polished to have the same angle of inclination of 8 to 12° with respect to a plane perpendicular to its optical axis corresponding to the angle of the terminal end of the above described ferrule.

The inclined surface 27 of the distributed refractive index lens 26 is brought into close contact with the inclined end surface 25 of the above described 4-core optical fiber ferrule F_1 . It is inserted into and bonded to a through hole 32 of a first alignment sleeve 30 having a short axial length capable of inserting about a half the axial length of the distributed refractive index rod lens 26. An integrally assembled, lens-incorporated ferrule

assembly L₁ is then formed. A lens-incorporated ferrule assembly L₂ is similarly formed.

Fig.4 is a sectional view showing an embodiment of a second alignment sleeve which constitutes a part of holding means of an embodiment of optical coupler according to the present invention. As will be described later, the second alignment sleeve 31 is a sleeve for receiving the two distributed refractive index rod lens 26, 26' to bring them into an alignment by causing a coincidence of their optical axes.

Fig.5 is a sectional view of a mirror coating and a glass plate for supporting the coating for use in a first embodiment of optical coupler according to the present invention. As shown in Fig.5, a mirror coating 29 imparted with reflectance and transmittance that are different according to the wavelength is applied to one face of a thin plate glass 28.

As shown in Fig.6, the first optical coupler according to the present invention is assembled such that a pair of optical elements shown in Fig.3 sandwiches the thin plate glass 28 for supporting the mirror coating 29 shown in Fig.5 by using the second alignment sleeve 31 shown in Fig.4.

The first alignment sleeves 30, 30' are the alignment sleeves for receiving the 4-core, optical fiber incorporated ferrules F₁, F₂ and the distributed refractive index rod lenses 26, 26', respectively, to align their optical axes.

In other words, in the state where the glass plate 28 is placed between the perpendicular end surfaces 33, 33' of the distributed refractive index lenses 26, 26' of the lens-incorporated ferrule assemblies L₁ and L₂, the insertion into the second alignment sleeve 31 is made such that the respective end surfaces are in close contact with one another.

Thereafter, the lens-incorporated ferrule assembly L₂ is rotated for adjustment to cause the optical axes of the optical fibers thereof to coincide the symmetrical positions of the optical fibers of the lens-incorporated ferrule assembly L₁. The distributed refractive index rod lenses 26, 26' are then fixed by means of adhesion to the through hole of the second alignment sleeve 31.

The operation of the embodiment shown in Fig.6 will now be described with reference to Fig.7.

Fig.7 illustrates the relation between the opposing optical fibers in the above described embodiment. The reflectance and transmittance of the mirror plate 28 with respect to wavelengths λ₁, λ₂ are selected such that λ₁ is reflected while λ₂ is transmitted.

Rays of wavelengths λ₁, λ₂ having passed through the optical fiber 21 may be demultiplexed and guided to the optical fibers 22' and 22, respectively. Conversely, by reversing the direction of a light beam, a ray of wavelength λ₁ in the optical fiber 22' and a ray of wavelength λ₂ in the optical fiber 22 may be multiplexed into the optical fiber 21. That is, a 1×2 circuit optical wave demultiplexer/multiplexer may be constructed. The optical fibers 23, 24, 21', 23', 24' are not used and these

function as dummies for the alignment of the optical fibers 21, 22, 22'.

Further, rays of wavelengths λ₁, λ₂ having passed through the optical fiber 23 may be demultiplexed and guided to the optical fibers 24' and 24, respectively. In this case, two sets of 1×2 circuit optical wave demultiplexer/multiplexer may be constructed.

The optical fibers to be used as "dummy" in achieving an alignment may be cut off at the rear end portion of the ferrule after its assembly.

A second embodiment of optical fiber ferrule according to the present invention will now be described with reference to Fig.8. Fig.8 is an enlarged sectional view of a terminal end portion of the optical fiber ferrule.

Fig.9 is a sectional view showing an embodiment of optical coupler using the optical fiber ferrule as shown in Fig.8. Those portions having similar functions as in the embodiment of optical coupler shown in Fig.6 are denoted by the same reference numerals.

Fig.8 is a sectional view of N-core ferrule which may be a constituent part of N/2 (N=8) sets of 1×2 circuit optical coupler.

It is now supposed that, in general, N (an even number of 6 or larger) uncovered optical fibers each having a diameter d₁ are disposed within a terminal end inner diameter d_N of N-core ferrule 34 with the optical fiber cores being on a concentric circle. An auxiliary rod 35 is then inserted into the center portion of the ferrule and is tightly secured therein. At this time, the inner diameter of the ferrule terminal end d_N, the diameter of an uncovered optical fiber d₁ and the outer diameter of the auxiliary rod d₀ are set to hold the following relationship:

$$d_N = d_1[(1/\sin\pi/N) + 1] + \delta \quad (1)$$

$$d_0 = d_1[(1/\sin\pi/N) - 1] \quad (2)$$

In equation (1), δ represents an error.

When N = 6, the outer diameter of the auxiliary rod d₀ is equal to d₁. In such case, an uncovered optical fiber may be used as the auxiliary rod.

Fig.9 is a sectional view showing an embodiment of optical coupler using the optical fiber ferrule shown in Fig.8. In this figure, a first alignment sleeve 30, 30' has a similar function as the above described first sleeve and serves to dispose the distributed refractive index rod lens 26, 26' at the terminal end of ferrule 34, 34'.

A mirror coating 29 is provided on a glass plate 28 and the glass plate 28 is supported between the distributed refractive index rod lenses 26, 26' by means of a second alignment sleeve 31.

The ferrule 34 and the distributed refractive index rod lens 26 are inserted into the first alignment sleeve 30 with an accurate correspondence of their optical axes to make a pair of lens-incorporated ferrules. The portion of the distributed refractive index rod lens 26, 26' extended from the first alignment sleeve 30, 30' of the lens-incorporated ferrule may be inserted into the

through hole of the second alignment sleeve 31 to achieve an accurate coincidence of the center of optical axes of all the components. One of the lens-incorporated ferrules is rotated to adjust the angle in the circumferential direction.

It is supposed here that the mirror coating 29 of the glass plate 28 reflects an optical wavelength component λ_1 and transmits an optical wavelength component λ_2 . Of a light beam consisting of wavelengths λ_1, λ_2 having passed through the optical fiber 40, rays of wavelength λ_1 are separated and guided to the optical fiber 44 and rays of λ_2 are separated and guided to the optical fiber 44'. By connecting a ray of wavelength λ_1 to optical fiber 44 and a ray of wavelength λ_2 to optical fiber 44', they are multiplexed into the optical fiber 40. In other words, $8/2=4$ circuits of 1×2 -circuit optical wave demultiplexer/multiplexer may be constructed with this embodiment. In general, $N/2$ circuits of optical wave demultiplexer/multiplexer may be constructed by using an optical fiber ferrule having N cores.

The outer diameter of each ferrule of the optical coupler according to the present invention may be precisely processed by using its center hole as a reference. It may be processed to precisely correspond to the outer diameter of a distributed refractive index lens. Both an alignment of optical axes and angular adjustment are easy. The ability required in its assembling operation is an equivalent to that for an ordinary optical connector assembly so that a skill such as the one in the conventional example is not necessary, and a great reduction in man-hour for assembly is possible. Further, with the second optical coupler, it is possible to integrally incorporate $N/2$ sets of 1×2 circuit optical wave demultiplexer/multiplexer or light branching/coupling devices so that the size and weight of the system may be reduced to result a great economical advantage.

Claims

1. An optical fiber ferrule (16) comprising optical fibers (21-24) being inserted into and fixed in a hole (17) at a terminal end of the ferrule (16) to cause the ends of four uncovered optical fibers (21-24) closely adjoining one another to be exposed, the terminal end being polished into a surface (25) slightly inclined by an angle θ with respect to a plane perpendicular to the axis of the ferrule.
2. An optical fiber ferrule (16) according to claim 1 wherein the following relation holds between the inner diameter of said ferrule and the outer diameter of the uncovered optical fiber and wherein the angle of inclination θ is 8 to 12°:

$$d = (2^{1/2} + 1)d_1 + \delta$$

where d is the inner diameter of the ferrule (16), d_1 is the diameter of each uncovered optical fiber (21-24) and δ represents an error.

3. An optical coupler comprising:

first and second optical fiber ferrules (16, 16') each comprising optical fibers inserted into and fixed in a hole at a terminal end of the ferrule so as to cause the respective ends of four uncovered optical fibers closely adjoining one another to be exposed, the terminal end being polished into a surface slightly inclined by an angle θ with respect to a plane perpendicular to the axis of the ferrule;

first and second distributed refractive index rod lenses (26, 26') each having one end surface polished to have an inclination θ with respect to the optical axis thereof;

a mirror coating layer (29) reflecting a portion of and transmitting another portion of a light beam incident thereon; and

a holding means (30, 30', 31) for bringing the respective inclined surfaces (27) of said first ferrule (16) and first distributed refractive index rod lens (26) into close contact to each other, bringing the respective inclined surfaces of said second ferrule (16') and second distributed refractive index rod lens (26') into close contact to each other, disposing said mirror coating layer (29) between said first and second distributed refractive index lenses (26, 26'), and coaxially holding the first and second optical fiber ferrules (16, 16'), the first and second distributed refractive index rod lenses (26, 26') and the mirror coating layer (29).

4. An optical coupler according to claim 3 wherein the outer diameter of said ferrule (16, 16') and the outer diameter of the distributed refractive index lens (26, 26') are substantially the same and said holding means (30, 30', 31) is provided as a circular cylinder having a corresponding inner diameter.
5. An optical fiber ferrule (34, 34') comprising N (an even number of 6 or larger) uncovered optical fibers (40, 40', 44, 44') being fixed in close contact to the inner circumferential surface at a terminal end of the ferrule (34, 34') and an auxiliary rod (35) inserted into the center thereof to position the optical fiber cores on a concentric circle, wherein the following relations hold among said ferrule terminal end inner diameter, the diameter of the uncovered optical fiber (40, 40', 44, 44') and the outer diameter of the auxiliary rod (35):

$$d_N = d_1 [(1/\sin(\pi/N)) + 1] + \delta$$

$$d_0 = d_1 [(1/\sin(\pi/N)) - 1]$$

where d_N is the inner diameter of the ferrule (34, 34'), d_1 is the diameter of each uncovered opti-

cal fiber (40, 40', 44, 44'), d_0 is the outer diameter of the auxiliary rod (35), and δ represents an error.

6. An optical coupler comprising:

first and second optical fiber ferrules (34, 34')
as claimed in claim 5;
first and second distributed refractive index
optical lenses (26, 26');
a mirror coating layer (29) reflecting a portion of
and transmitting another portion of a light beam
incident thereon; and
a holding means (30, 30', 31) for bringing said
first ferrule (34) and the first distributed refrac-
tive index rod lens (26) into close contact to
each other, bringing said second ferrule (34')
and the second distributed refractive index rod
lens (26') into close contact to each other, dis-
posing said mirror coating layer (29) between
said first and second distributed refractive
index lenses (26, 26'), and coaxially holding the
first and second optical fiber ferrules (34, 34'),
the first and second distributed refractive index
rod lenses (26, 26'), and the mirror coating
layer (29).

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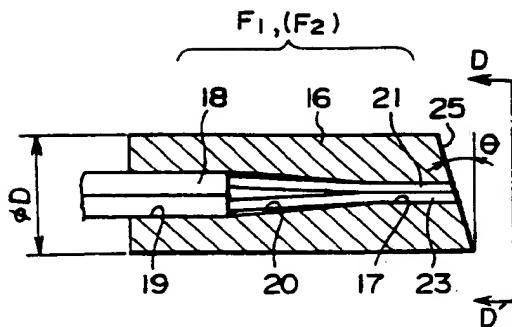
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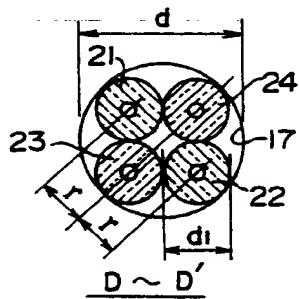
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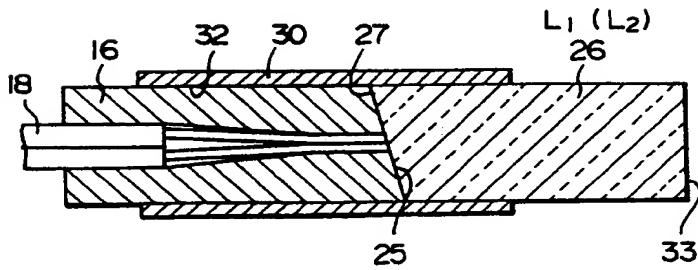
F I G. 1



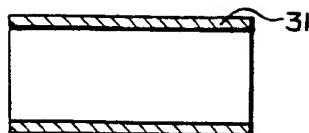
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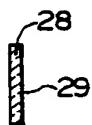
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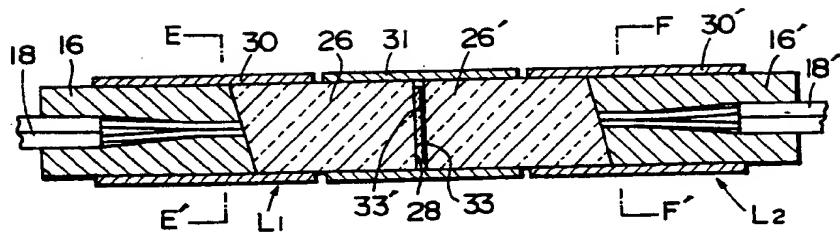
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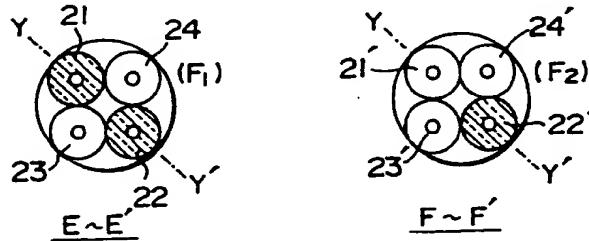
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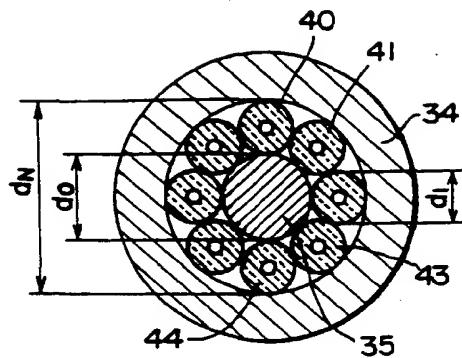
F I G. 6



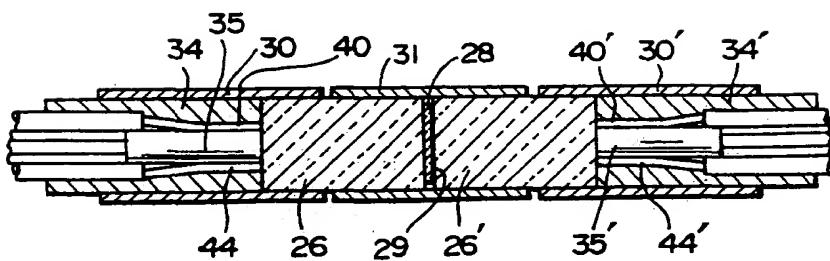
F I G. 7



F I G. 8

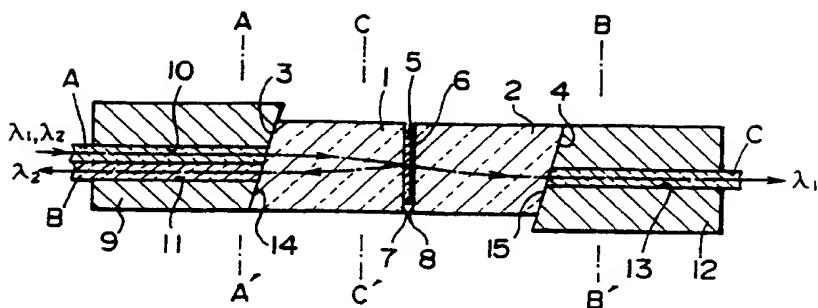


F I G. 9



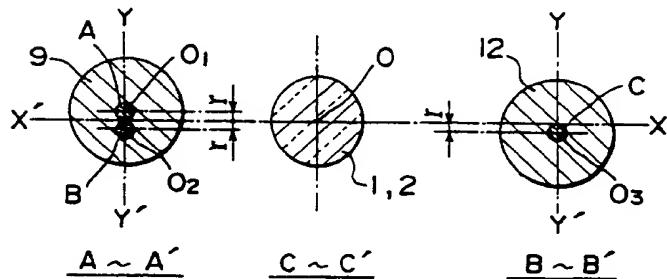
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European Patent
Office

EUROPEAN SEARCH REPORT

Application Number
EP 96 10 5950

DOCUMENTS CONSIDERED TO BE RELEVANT

Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.)
X	EP-A-0 439 312 (ADC TELECOMMUNICATIONS INC) 31 July 1991 * column 3, line 45 - column 4, line 5; figures 3,4 *	1	G02B6/38 G02B6/34 G02B26/02
Y	* column 3, line 32 - line 34 *	3	
Y	* column 4, line 4 - line 14 *	2	
Y	---	4	
Y	GB-A-2 218 222 (ADC TELECOMMUNICATIONS LTD) 8 November 1989 * page 3, line 20 - line 31 * * page 13, line 26 - line 31 * ---	3	
Y	US-A-5 377 286 (IIDA MASANORI ET AL) 27 December 1994 * column 11, line 26 - line 28 * ---	2	
Y	US-A-4 213 677 (ISHIKAWA RO ET AL) 22 July 1980 * column 3, line 7 - column 4, line 7 * * column 6, line 9 - line 26; figures 1,6 *	3,4,6	
X	US-A-4 208 094 (TOMLINSON WALTER J III ET AL) 17 June 1980 * column 4, line 64 - column 5, line 25; figure 6 *	5	GO2B
Y	---	6	
A	PATENT ABSTRACTS OF JAPAN vol. 009, no. 174 (P-374), 19 July 1985 & JP-A-60 048004 (MITSUBISHI DENKI KK), 15 March 1985, * abstract *	3	
A	US-A-4 733 931 (FAN ROBERT J) 29 March 1988 * the whole document *	3,4,6	
The present search report has been drawn up for all claims			
Place of search	Date of completion of the search	Examiner	
MUNICH	25 July 1996	Lord, R	
CATEGORY OF CITED DOCUMENTS			
X : particularly relevant if taken alone	T : theory or principle underlying the invention		
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